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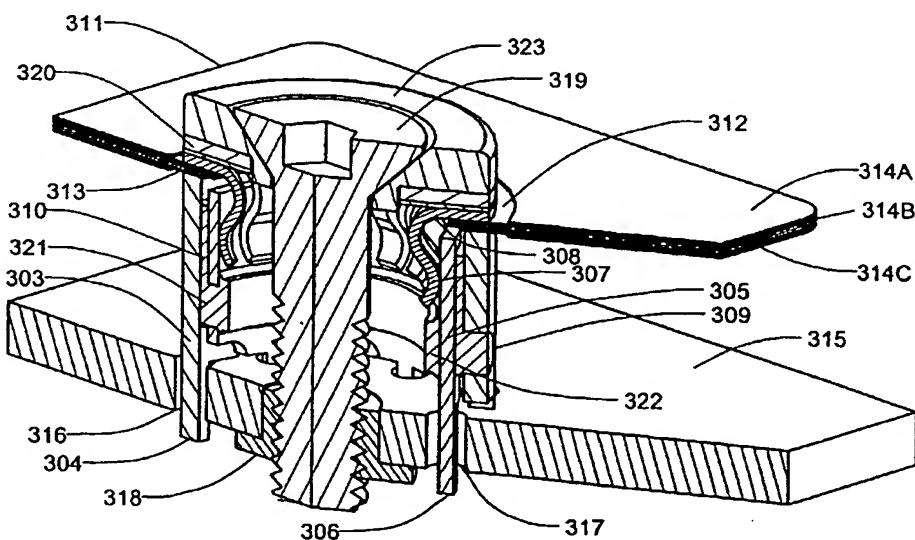
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(54) Title: SEPARABLE POWER DELIVERY CONNECTOR



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(57) Abstract: A connector for providing power from a first circuit board to a second circuit board. The apparatus comprises a first conductive member, including a first conductive member first end and a first conductive member second end distal from the first end; a second conductive member disposed within the first conductive member, the second conductive member including a second conductor member first end and a second conductor member second end distal from the second conductor member first end; and one or more first circuit board permanent attachment features for electrical coupling with the first circuit board and second circuit board, and one or more disconnectable conduction features for electrically coupling the connector with the second circuit board.



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SEPARABLE POWER DELIVERY CONNECTOR

CROSS-REFERENCE TO RELATED APPLICATIONS

This application claims benefit of the following provisional patent applications, which are hereby incorporated by reference herein:

- Application Serial No. 60/287,860, entitled "POWER TRANSMISSION DEVICE," by Joseph T. DiBene II, David H. Hartke, Carl E. Hoge, and Edward J. Derian, filed May 1, 2001;
- Application Serial No. 60/291,749, entitled "MICRO I-PAK ARCHITECTURE HAVING A FLEXIBLE CONNECTOR BETWEEN A VOLTAGE REGULATION MODULE AND SUBSTRATE," by Joseph T. DiBene II, filed May 16, 2001;
- Application Serial No. 60/291,772, entitled "I-PAK ARCHITECTURE POWERING MULTIPLE DEVICES," by Joseph T. DiBene II, David H. Hartke, Carl E. Hoge, and Edward J. Derian, filed May 16, 2001;
- Application Serial No. 60/292,125, entitled "VORTEX HEATSINK FOR LOW PRESSURE DROP HIGH PERFORMANCE THERMAL MANAGEMENT ELECTRONIC ASSEMBLY SOLUTIONS," by Joseph T. DiBene II, Farhad Raiszadeh, filed May 18, 2001;
- Application Serial No. 60/299,573, entitled "IMPROVED MICRO-I-PAK STACK-UP ARCHITECTURE," by Joseph T. DiBene II, Carl E. Hoge, and David H. Hartke, filed June 19, 2001;
- Application Serial No. 60/301,753, entitled "INTEGRATED POWER DELIVERY USING HIGH PERFORMANCE LINEAR REGULATORS ON PACKAGE WITH A MICROPROCESSOR," by Joseph T. DiBene II, Carl E. Hoge, and David H. Hartke, filed June 27, 2001;
- Application Serial No. 60/304,929, entitled "BORREGO ARCHITECTURE," by David H. Hartke and Joseph T. DiBene II, filed July 11, 2001;

- Application Serial No. 60/304,930, entitled "MICRO-I-PAK," by Joseph T. DiBene II, Carl E. Hoge, David H. Hartke, and Edward J. Derian, filed July 11, 2001;
- Application Serial No. 60/310,038, entitled "TOOL-LESS CONCEPTS FOR BORREGO," by Edward J. Derian and Joseph T. DiBene II, filed August 3, 2001;
- 5 Application Serial No. 60/313,338, entitled "TOOL-LESS PRISM IPA ASSEMBLY TO SUPPORT IA64 MCKINLEY MICROPROCESSOR," by David H. Hartke and Edward J. Derian, filed August 17, 2001;
- Application Serial No. 60/338,004, entitled "MICRO-SPRING CONFIGURATIONS FOR POWER DELIVERY FROM VOLTAGE REGULATOR
- 10 MODULES TO INTEGRATED CIRCUITS AND MICROPROCESSORS," by Joseph T. DiBene II, David H. Hartke, Carl E. Hoge, and Edward J. Derian, filed November 8, 2001;
- Application Serial No. 60/361,554, entitled "RIGHT ANGLE POWER CONNECTOR ARCHITECTURE," by David H. Hartke, filed March 4, 2002; and
- 15 Application Serial No. 60/359,504, entitled "HIGH EFFICIENCY VRM CIRCUIT CONSTRUCTIONS FOR LOW VOLTAGE, HIGH CURRENT ELECTRONIC DEVICES," by Philip M. Harris, filed February 25, 2002,
- This patent application is also continuation-in-part of the following co-pending and commonly assigned patent applications, each of which applications are hereby
- 20 incorporated by reference herein:
- Application Serial No. 09/885,780, entitled "INTER-CIRCUIT ENCAPSULATED PACKAGING," by Joseph T. DiBene II and David H. Hartke, filed June 19, 2001, which is a continuation in-part of application Serial No. 09/353,428, entitled "INTER-CIRCUIT ENCAPSULATED PACKAGING," by
- 25 Joseph T. DiBene II and David H. Hartke, filed July 15, 1999 and now issued as U.S. Patent No. 6,304,450;
- Application Serial No. 09/432,878, entitled "INTER-CIRCUIT ENCAPSULATED PACKAGING FOR POWER DELIVERY," by Joseph T. DiBene

II and David H. Hartke, filed November 2, 1999, which is a continuation-in-part of Application Serial No. 09/353,428, entitled "INTER-CIRCUIT ENCAPSULATED PACKAGING," by Joseph T. DiBene II and David H. Hartke, filed July 15, 1999 and now issued as U.S. Patent No. 6,304,450;

5 Application Serial No. 09/727,016, entitled "EMI CONTAINMENT USING INTER-CIRCUIT ENCAPSULATED PACKAGING TECHNOLOGY" by Joseph T. DiBene II and David Hartke, filed November 28, 2000, which claims priority to the following U.S. Provisional Patent Applications:

10 Application Serial No. 60/167,792, entitled "EMI CONTAINMENT USING INTER-CIRCUIT ENCAPSULATED PACKAGING TECHNOLOGY," by Joseph T. DiBene II and David H. Hartke, filed November 29, 1999;

15 Application Serial No. 60/171,065, entitled "INTER-CIRCUIT ENCAPSULATED PACKAGING TECHNOLOGY," by Joseph T. DiBene II and David H. Hartke, filed December 16, 1999;

20 Application Serial No. 60/183,474, entitled "DIRECT ATTACH POWER/THERMAL WITH INCEP," by Joseph T. DiBene II and David H. Hartke, filed February 18, 2000;

25 Application Serial No. 60/187,777, entitled "NEXT GENERATION PACKAGING FOR EMI CONTAINMENT, POWER DELIVERY, AND THERMAL DISSIPATION USING INTER-CIRCUIT ENCAPSULATED PACKAGING TECHNOLOGY," by Joseph T. DiBene II and David H. Hartke, filed March 8, 2000;

30 Application Serial No. 60/196,059, entitled "EMI FRAME WITH POWER FEED-THROUGH AND THERMAL INTERFACE MATERIAL IN AN AGGREGATE DIAMOND MIXTURE," by Joseph T. DiBene II and David H. Hartke, filed April 10, 2000;

Application Serial No. 60/219,506, entitled "HIGH PERFORMANCE THERMAL MECHANICAL INTERFACE," by Wendell C. Johnson, David H. Hartke and Joseph T. DiBene II, filed July 20, 2000;

5 Application Serial No. 60/219,813, entitled "HIGH-CURRENT MICROPROCESSOR POWER DELIVERY SYSTEMS," by Joseph T. DiBene II, filed July 21, 2000;

10 Application Serial No. 60/222,386, entitled "HIGH DENSITY CIRCULAR 'PIN' CONNECTOR FOR HIGH SPEED SIGNAL INTERCONNECT," by David H. Hartke and Joseph T. DiBene II, filed August 2, 2000;

Application Serial No. 60/222,407, entitled "VAPOR HEAT SINK COMBINATION FOR HIGH EFFICIENCY THERMAL MANAGEMENT," by David H. Hartke and Joseph T. DiBene II, filed August 2, 2000; and

15 Application Serial No. 60/232,971, entitled "INTEGRATED POWER DISTRIBUTION AND SEMICONDUCTOR PACKAGE," by Joseph T. DiBene II, James J. Hjerpe, filed September 14, 2000;

Application Serial No. 09/785,892, entitled "METHOD AND APPARATUS FOR PROVIDING POWER TO A MICROPROCESSOR WITH INTEGRATED THERMAL AND EMI MANAGEMENT," by Joseph T. DiBene II, David H. Hartke, 20 James J. Hjerpe Kaskade, and Carl E. Hoge, filed February 16, 2001, which claims priority to the following Provisional Patent Applications;

Application Serial No. 60/183,474, entitled "DIRECT ATTACH POWER/THERMAL WITH INCEP," by Joseph T. DiBene II and David H. Hartke, filed February 18, 2000;

25 Application Serial No. 60/186,769, entitled "THERMACEP SPRING BEAM," by Joseph T. DiBene II and David H. Hartke, filed March 3, 2000;

Application Serial No. 60/187,777, entitled "NEXT GENERATION PACKAGING FOR EMI CONTAINMENT, POWER DELIVERY, AND

THERMAL DISSIPATION USING INTER-CIRCUIT ENCAPSULATED
PACKAGING TECHNOLOGY," by Joseph T. DiBene II and David H.
Hartke, filed March 8, 2000;

5 Application Serial No. 60/196,059, entitled "EMI FRAME WITH
POWER FEED-THROUGH AND THERMAL INTERFACE MATERIAL IN
AN AGGREGATE DIAMOND MIXTURE," by Joseph T. DiBene II and
David H. Hartke, filed April 10, 2000;

10 Application Serial No. 60/219,506, entitled "HIGH PERFORMANCE
THERMAL MECHANICAL INTERFACE," by Wendell C. Johnson, David
H. Hartke and Joseph T. DiBene II, filed July 20, 2000;

Application Serial No. 60/219,813, entitled "HIGH-CURRENT
MICROPROCESSOR POWER DELIVERY SYSTEMS," by Joseph T.
DiBene II, filed July 21, 2000;

15 Application Serial No. 60/222,386, entitled "HIGH DENSITY
CIRCULAR 'PIN' CONNECTOR FOR HIGH SPEED SIGNAL
INTERCONNECT," by David H. Hartke and Joseph T. DiBene II, filed
August 2, 2000;

20 Application Serial No. 60/222,407, entitled "VAPOR HEAT SINK
COMBINATION FOR HIGH EFFICIENCY THERMAL MANAGEMENT,"
by David H. Hartke and Joseph T. DiBene II, filed August 2, 2000; and

Application Serial No. 60/232,971, entitled "INTEGRATED POWER
DISTRIBUTION AND SEMICONDUCTOR PACKAGE," by Joseph T.
DiBene II, James J. Hjerpe, filed September 14, 2000;

25 Application Serial No. 60/251,222, entitled "INTEGRATED POWER
DELIVERY WITH FLEX CIRCUIT INTERCONNECTION FOR HIGH
DENSITY POWER CIRCUITS FOR INTEGRATED CIRCUITS AND
SYSTEMS," by Joseph T. DiBene II and David H. Hartke, filed December 4,
2000;

Application Serial No. 60/251,223, entitled "MICRO I-PAK FOR POWER DELIVERY TO MICROELECTRONICS," by Joseph T. DiBene II and Carl E. Hoge, filed December 4, 2000;

5 Application Serial No. 60/251,184, entitled "MICROPROCESSOR INTEGRATED PACKAGING," by Joseph T. DiBene II, filed December 4, 2000; and

10 Application Serial No. 60/266,941, entitled "MECHANICAL INTERCONNECTION TECHNOLOGIES USING FLEX CABLE INTERCONNECT FOR DELIVERY IN 'INCEP' INTEGRATED ARCHITECTURE," by David H. Hartke, James M. Broder, Joseph T. DiBene II, filed February 6, 2001;

15 Application Serial No. 09/798,541, entitled "THERMAL/MECHANICAL SPRINGBEAM MECHANISM FOR HEAT TRANSFER FROM HEAT SOURCE TO HEAT DISSIPATING DEVICE," by Joseph T. DiBene II, David H. Hartke, Wendell C. Johnson, and Edward J. Derian, filed March 2, 2001, which is a continuation-in-part of Application Serial No. 09/727,016, entitled "EMI CONTAINMENT USING INTER-CIRCUIT ENCAPSULATED PACKAGING TECHNOLOGY," by Joseph T. DiBene II and David H. Hartke, filed November 28, 2000, and a continuation-in-part of Application Serial No. 09/785,892, entitled
20 "METHOD AND APPARATUS FOR PROVIDING POWER TO A MICROPROCESSOR WITH INTEGRATED THERMAL AND EMI MANAGEMENT," by Joseph T. DiBene II and David H. Hartke, filed February 16, 2001, and a continuation in part of Application Serial No. 09/432,878, entitled "INTER-CIRCUIT ENCAPSULATED PACKAGING FOR POWER DELIVERY",
25 by Joseph T. DiBene II and David H. Hartke, filed November 2, 1999, which is a continuation in part of Application Serial No. 09/353,428, entitled "INTER-CIRCUIT ENCAPSULATED PACKAGING," by Joseph T. DiBene II and David H. Hartke,

filed July 15, 1999 and now issued as U.S. Patent No. 6,304,450, and which claims priority to the following U.S. Provisional Patent Applications:

- Application Serial No. 60/183,474, entitled "DIRECT ATTACH POWER/THERMAL WITH INCEP," by Joseph T. DiBene II and David H. Hartke, filed February 18, 2000;
- Application Serial No. 60/186,769, entitled "THERMACEP SPRING BEAM," by Joseph T. DiBene II and David H. Hartke, filed March 3, 2000;
- Application Serial No. 60/187,777, entitled "NEXT GENERATION PACKAGING FOR EMI CONTAINMENT, POWER DELIVERY, AND THERMAL DISSIPATION USING INTER-CIRCUIT ENCAPSULATED PACKAGING TECHNOLOGY," by Joseph T. DiBene II and David H. Hartke, filed March 8, 2000;
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Application Serial No. 09/801,437, entitled "METHOD AND APPARATUS FOR DELIVERING POWER TO HIGH PERFORMANCE ELECTRONIC ASSEMBLIES" by Joseph T. DiBene II, David H. Hartke, Carl E. Hoge, James M. Broder, Edward J. Derian, Joseph S. Riel, and Jose B. San Andres, filed March 8, 2001, which is a continuation in part of the following patent applications:

Application Serial No. 09/798,541, entitled
“THERMAL/MECHANICAL SPRINGBEAM MECHANISM FOR HEAT
TRANSFER FROM HEAT SOURCE TO HEAT DISSIPATING DEVICE,”
by Joseph T. DiBene II, David H. Hartke, Wendell C. Johnson, and Edward J.
5 Derian, filed March 2, 2001;

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T. DiBene II, David H. Hartke, James J. Hjerpe Kaskade, and Carl E. Hoge,
filed February 16, 2001;

15 Application Serial No. 09/727,016, entitled “EMI CONTAINMENT
USING INTER-CIRCUIT ENCAPSULATED PACKAGING
TECHNOLOGY” by Joseph T. DiBene II and David Hartke, filed November
28, 2000;

20 Application Serial No. 09/432,878, entitled “INTER-CIRCUIT
ENCAPSULATED PACKAGING FOR POWER DELIVERY,” by Joseph T.
DiBene II and David H. Hartke, filed November 2, 1999, which is a
continuation-in-part of Application Serial No. 09/353,428, entitled “INTER-
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David H. Hartke, filed July 15, 1999 and now issued as U.S. Patent No.
6,304,450;

and which claims priority to the following U.S. Provisional Patent

Applications:

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- Application Serial No. 60/266,941, entitled "MECHANICAL INTERCONNECTION TECHNOLOGIES USING FLEX CABLE INTERCONNECT FOR POWER DELIVERY IN 'INCEP' INTEGRATED ARCHITECTURE," by David H. Hartke, James M. Broder, Joseph T. DiBene II, filed February 6, 2001;
- Application Serial No. 09/802,329, entitled "METHOD AND APPARATUS FOR THERMAL AND MECHANICAL MANAGEMENT OF A POWER REGULATOR MODULE AND MICROPROCESSOR IN CONTACT WITH A THERMALLY CONDUCTING PLATE" by Joseph T. DiBene II and David H. Hartke, filed March 8, 2001, which is a continuation in part of the following patent applications:
- Application Serial No. 09/798,541, entitled "THERMAL/MECHANICAL SPRINGBEAM MECHANISM FOR HEAT TRANSFER FROM HEAT SOURCE TO HEAT DISSIPATING DEVICE," by Joseph T. DiBene II, David H. Hartke, Wendell C. Johnson, and Edward J. Derian, filed March 2, 2001, which is a continuation-in-part of Application Serial No. 09/727,016, entitled "EMI CONTAINMENT USING INTER-CIRCUIT ENCAPSULATED PACKAGING TECHNOLOGY," by Joseph T. DiBene II and David H. Hartke, filed November 28, 2000, and a continuation-in-part of Application Serial No. 09/785,892, entitled "METHOD AND APPARATUS FOR PROVIDING POWER TO A MICROPROCESSOR WITH INTEGRATED THERMAL AND EMI MANAGEMENT," by Joseph T. DiBene II and David H. Hartke, filed February 16, 2001, and a continuation in part of Application Serial No. 09/432,878, entitled "INTER-CIRCUIT ENCAPSULATED PACKAGING FOR POWER DELIVERY", by Joseph T. DiBene II and David H. Hartke, filed November 2, 1999, which is a continuation in part of Application Serial No. 09/353,428, entitled "INTER-CIRCUIT ENCAPSULATED PACKAGING," by Joseph T. DiBene II and

David H. Hartke, filed July 15, 1999 and now issued as U.S. Patent No. 6,304,450;

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and which claims priority to the following U.S. Provisional Patent

20 Applications:

Application Serial No. 60/187,777, entitled "NEXT GENERATION PACKAGING FOR EMI CONTAINMENT, POWER DELIVERY, AND THERMAL DISSIPATION USING INTER-CIRCUIT ENCAPSULATED PACKAGING TECHNOLOGY," by Joseph T. DiBene II and David H.

25 Hartke, filed March 8, 2000;

Application Serial No. 60/196,059, entitled "EMI FRAME WITH POWER FEED-THROUGH AND THERMAL INTERFACE MATERIAL IN

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10 Application Serial No. 60/222,407, entitled "VAPOR HEAT-SINK COMBINATION FOR HIGH EFFICIENCY THERMAL MANAGEMENT," by David H. Hartke and Joseph T. DiBene II, filed August 2, 2000;

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Application Serial No. 60/266,941, entitled "MECHANICAL INTERCONNECTION TECHNOLOGIES USING FLEX CABLE

INTERCONNECT FOR POWER DELIVERY IN ‘INCEP’ INTEGRATED ARCHITECTURE,” by David H. Hartke, James M. Broder, Joseph T. DiBene II, filed February 6, 2001;

Application Serial No. 09/910,524, entitled “HIGH PERFORMANCE

- 5 THERMAL/MECHANICAL INTERFACE FOR FIXED-GAP REFERENCES FOR HIGH HEAT FLUX AND POWER SEMICONDUCTOR APPLICATIONS”, by Joseph T. DiBene II, David H. Hartke, Wendell C. Johnson, Farhad Raiszadeh, Edward J. Darien and Jose B. San Andres, filed July 20, 2001, which is a continuation in part of the following patent applications:

10 Application Serial No. 09/801,437, entitled “METHOD AND APPARATUS FOR DELIVERING POWER TO HIGH PERFORMANCE ELECTRONIC ASSEMBLIES” by Joseph T. DiBene II, David H. Hartke, Carl E. Hoge, James M. Broder, Edward J. Derian, Joseph S. Riel, and Jose B. San Andres, filed March 8, 2001;

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continuation-in-part of Application Serial No. 09/353,428, entitled "INTER-
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- 15 Application Serial No. 60/292,125, entitled "VORTEX HEAT SINK FOR LOW PRESSURE DROP HIGH PERFORMANCE THERMAL MANAGEMENT ELECTRONIC ASSEMBLY SOLUTIONS," by Joseph T. DiBene II and Farhad Raiszadeh, filed May 18, 2001;
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Application Serial No. 09/818,173, entitled "INTER-CIRCUIT

- 5 ENCAPSULATED PACKAGING," by David H. Hartke and Joseph T. DiBene II, filed March 26, 2001, which is a continuation in part of the following patent applications:

Application Serial No. 09/801,437, entitled "METHOD AND APPARATUS FOR DELIVERING POWER TO HIGH PERFORMANCE 10 ELECTRONIC ASSEMBLIES" by Joseph T. DiBene II, David H. Hartke, Carl E. Hoge, James M. Broder, Edward J. Derian, Joseph S. Riel, and Jose B. San Andres, filed March 8, 2001;

15 Application Serial No. 09/802,329, entitled "METHOD AND APPARATUS FOR THERMAL AND MECHANICAL MANAGEMENT OF A POWER REGULATOR MODULE AND MICROPROCESSOR IN CONTACT WITH A THERMALLY CONDUCTING PLATE" by Joseph T. DiBene II and David H. Hartke, filed March 8, 2001;

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- 20 Application Serial No. 60/299,573, entitled "MICRO I-PAK STACK UP ARCHITECTURE," by Joseph T. DiBene II, Carl E. Hoge, and David H. Hartke, filed June 19, 2001;
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20 Application Serial No. 10/036,957, entitled "ULTRA-LOW IMPEDANCE POWER INTERCONNECTION SYSTEM FOR ELECTRONIC PACKAGES," by Joseph T. DiBene II, David H. Hartke, Carl E. Hoge, and Edward J. Derian, filed December 20, 2001, which is a continuation-in-part of the following patent applications:

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BACKGROUND OF THE INVENTION

1. Field of the Invention

15 This invention relates in general to power distribution delivered to high performance circuits, and in particular to a system and method for distributing power to one or more circuit boards while providing for improved packaging.

2. Description of the Related Art

20 As electronic circuits become more complex, packaging of the circuitry has become more difficult. The common method for packaging integrated circuits (ICs) and other electronic components is to mount them on printed circuit boards (PCBs) or other substrates such as ceramic or organic consisting of alternating conductive and non-conductive layers or planes sandwiched or bonded together to form a dense X-Y
25 signal interconnect. For a number of years, the operating voltage of ICs was approximately 5 volts and the power consumption was generally less than 1 watt. This relatively high supply voltage and low power level allowed the packaging of a

large number of ICs on a single PCB with power distribution incorporated into one or more of the PCB planes.

More recently, advances in silicon fabrication techniques have permitted the manufacture of high performance IC packages with operating voltages at or below 1 volt and power levels in excess of 100 watts. As described in co-pending and commonly assigned patent application serial number 09/785,892, METHOD AND APPARATUS FOR PROVIDING POWER TO A MICROPROCESSOR WITH INTEGRATED THERMAL AND EMI MANAGEMENT, by Joseph T. DiBene II et. al., filed February 16, 2001, which application is hereby incorporated by reference, the transient current to some of these packages can approach hundreds of amps per microsecond. To assure optimum performance under these conditions, what is needed is a design which provides an electrical path from the power supply or voltage regulation module (VRM) to the IC that accommodates both high current flow and low series inductance, two goals are difficult to achieve at the same time.

The present invention achieves both of these goals, while also allowing for a compact, integrated stack-up system design that permits thermal dissipation and control of electromagnetic interference (EMI).

SUMMARY OF THE INVENTION

To address the requirements described above, the present invention discloses a method, apparatus, and article of manufacture, for providing power from a first circuit board to a second circuit board. The apparatus comprises a first conductive member, including a first conductive member first end and a first conductive member second end distal from the first end; a second conductive member disposed within the first conductive member, the second conductive member including a second conductor member first end and a second conductor member second end distal from the second conductor member first end; and one or more first circuit board permanent attachment features for electrical coupling with the first circuit board and second circuit board,

and one or more disconnectable conduction features for electrically coupling the connector with the second circuit board. One of the advantages of the present invention is the integration of function in which the apparatus operates both as a rigid standoff to separate the first circuit board from the second circuit board, and a conduit 5 for delivering power and a ground return between the circuit boards as well. While the apparatus will be discussed in terms of providing a power signal from a first circuit board to a second circuit board, it can also be used to provide power to a plurality of circuit boards in a stacked configuration, all with minimal interconnect impedance.

10

BRIEF DESCRIPTION OF THE DRAWINGS

Referring now to the drawings in which like reference numbers represent corresponding parts throughout:

FIG. 1A is a two-dimensional section view illustrating an architecture in which 15 the present invention may be usefully employed in delivering power to an electronic device such as a microprocessor;

FIG. 1B is a section view of a microprocessor package used in FIG. 1A which further illustrates the location of the able power connectors associated with delivering power to the microprocessor shown if FIG. 1A;

20 FIG. 2A is a two-dimensional section view of a conceptual coaxial interconnect illustrating the delivery of electrical energy from an upper planar circuit structure to a lower planar circuit structure;

FIG. 2B is a two-dimensional plan view of the current flow to the coaxial interconnect structure in the upper planar circuit of FIG. 2A;

25 FIG. 3A is an exploded isometric view of a coaxial power connection method utilizing an inner diameter contact washer as a method of connecting the inner cylinder of the connector to a flexible PCB;

FIG. 3B is an isometric section view of the structure shown in FIG. 3A together with an upper flexible PCB, a lower rigid PCB and the associated fasteners and assembly washers;

5 FIG. 4A is an exploded isometric view of a coaxial power connector illustrating the outer shell, dielectric insulator and inner shell;

FIG. 4B is an isometric view of the assembled coaxial power connector illustrated in FIG. 4A;

4 FIG. 4C is an isometric section view of the structure shown in FIGs. 4A and 4B together with an upper PCB, a lower PCB and the associated fastener and
10 assembly washers;

FIG. 5A is an exploded isometric view of a coaxial power connection method utilizing dual interdigitated spring finger contacts which are a part of the inner and outer cylinders and are used as a method of connecting the inner and outer cylinders of the connector to a PCB;

15 FIG. 5B is an isometric view of the assembled coaxial power connector illustrated in FIG. 5A ; and

FIG. 5C is an isometric section view of the structure shown in FIGs. 5A and 5B together with an upper PCB, a lower PCB and the associated fastener and assembly washer.

20 DETAILED DESCRIPTION OF PREFERRED EMBODIMENTS

In the following description, reference is made to the accompanying drawings which form a part hereof, and which is shown, by way of illustration, several embodiments of the present invention. It is understood that other embodiments may be utilized and structural changes may be made without departing from the scope of
25 the present invention.

Overview

The present invention discloses a separable coaxial connector for providing power from a first circuit board to a second circuit board. In one embodiment, the apparatus comprises an inner cylindrical cylinder, an intermediate coaxially located insulator or dielectric material and an outer coaxially located cylindrical cylinder. The connector is disposed between a first planar structure or printed circuit board and a second planar structure or printed circuit board to provide a path for the transfer of electrical power and a ground return between the two planar structures in an efficient manner. This creates a very low impedance interconnect between power planes on the first planar structure and power planes on the second planar structure.

The present invention discloses a variety of methods in which the separable coaxial cylinders of the connector assembly may be joined to the upper and lower planar structures.

The present invention further describes a specific application where the separable coaxial connector assembly may be especially beneficial to delivering power to high performance microprocessor packages in such a manner as to negate the need to integrate power regulation circuitry directly onto the microprocessor package (hereinafter referred to as On-Package-Voltage-Regulation, OPVR), so as to improve the producibility, yield and cost of modern high performance microprocessors.

20

Encapsulated Circuit Assembly

Typically, a modern high performance microprocessor die is flip-chip attached to an organic or ceramic substrate utilizing a Controlled-Collapse-Chip-Connection (C4). The substrate has power planes which are used to distribute power to the chip connections. Often, the power requirements of the microprocessor exceed 100 watts at operating voltages of approximately 1 volt and transient current requirements in excess of 1000 amps per microsecond. Typically, power conditioning is required to transform system power (which is usually high voltage and low current) to lower

voltages and higher current. Such power conditioning can be provided by a VRM. The stringent power demands require that the VRM be very closely coupled to the microprocessor or directly mounted onto the microprocessor substrate (the direct-mounting configuration is often called On-Package-Voltage-Regulation (OPVR)).

5 OPVR architectures require combining VRM technology with high performance silicon technology all on a common substrate which is often very expensive because of the very large number of layers required to manage both the power and signal interconnect to the microprocessor die. The resulting assembly has reduced yield and higher costs than what might be achieved if the microprocessor function could be

10 separated from the VRM function without reducing performance.

FIG. 1A is a diagram of a stack up assembly 100 illustrating the use of a coaxial connector assembly 105 used to deliver power to a microprocessor substrate 101 and its associated lid 108 from a remotely located VRM assembly 102. The VRM assembly 102 may include components 110 mounted on a VRM circuit board 114 and interconnected with other components on the circuit board 114 by circuit traces 112 in or on the circuit board 114. In the illustrated embodiment, the VRM assembly 102 surrounds the microprocessor lid 108, thus saving space in the z (vertical) axis.

The microprocessor lid 108 is thermally coupled to a heatsink structure 106 through a thermal coupling mesa 107 and appropriate thermal interface material (TIM) such as thermal grease (not shown) which can be integral to the base of 107 or a separate structure that is coupled (i.e. bonded, or metallically fused) to the base of the heatsink structure 106. Furthermore, heat generated from components in the VRM assembly 102 can be thermally attached directly to the base of heatsink assembly 106, thus sharing the heat dissipation benefits of the heatsink assembly 106. Signals from the microprocessor can be connected through pins (not shown) to socket 104 which is mounted to main board 103.

Power from the VRM assembly 102 is efficiently coupled to the microprocessor substrate 101 by utilizing one or more coaxial power connector assemblies 105. In one embodiment, four coaxial power connector assemblies 105 are used, and each is located proximate a corner of the microprocessor substrate 101.

5 FIG. 1B is a diagram showing the location of the four coaxial power connector assemblies 105 proximate the corners of the microprocessor substrate 105. The coaxial power connector assemblies 105 may be located in other locations on the substrate 101 such as at the center of each side. Further, the number of coaxial power connector assemblies 105 used can be varied to meet the power needs of target
10 microprocessor or other high performance integrated circuit assemblies.

Coaxial Interconnect

FIGs. 2A and 2B are diagrams illustrating a system for transfer of energy from a source (such as a VRM) on a first circuit board 201 to a second circuit board 202 through a coaxial power connector assembly 203.

A power signal 211 supplying current flows from the VRM on the first circuit board 201 (hereinafter alternatively referred to as first PCB) through a conductive plane 204 in or on the first circuit board 201 through plated-through-holes (PTHs) 213 to an isolated surface pad 214 on the bottom surface of first circuit board 201 thence
20 through interface connection 215A to coaxial power connector assembly 203. The power signal then passes through the first conductive member 209 to similar connections on the second circuit board 202 and then onto conductive plane 207 in or on the second circuit board 202, and thence to the load (e.g. the IC or microprocessor). A ground return signal 212 passes from a ground plane 206 in or on the second circuit
25 board 202 through interface connection 215B to a second conductive member 208 , through the second conductive member 208, through interface connection 215 and, finally, to conductive plane 205 on or in the first circuit board 201. This acts as a ground return for the VRM power signal. The space between the first conductive

member 209 and the second conductive member 208 may include a dielectric or electric insulator 210, if desired.

The interface connections 215 represent an electro-mechanical connection between the coaxial cylinders 208 and 209 and the circuit board features 205, 206 and 214. These connections may be a continuous interface such as may occur if the coaxial cylinders were to be soldered or pressed directly onto the conductive planes of board 201 and 202. However, there may be instances where discrete or separate connections to the boards 201 and 202 may be desirable. Such would be the case if the connections were spring fingers or formed leads on one or both of the cylinders 10 208 and 209. When discrete connections are utilized it is important that such connections be placed uniformly around the circumference of the cylinders so that the current flows substantially equally through the walls of the coaxial cylinders. When both cylinders utilize discrete connections then it is very desirable that these connections be alternated (one polarity being disposed adjacent another polarity on 15 both sides) in an interdigitated fashion to achieve the lowest interconnect inductance from the planes of the boards 201 and 202 and the cylinders 208 and 209 of coaxial connector assembly 203. FIG. 2B illustrates such an arrangement where the interface connections 215 are arranged in a uniform manner around the perimeters of the coaxial cylinders. Then, source current 211 and sink current 212 are meant to 20 illustrate a substantially uniform current distribution into and out of the cylinders.

In a preferred embodiment, the second conductive member 208 is hollow and the first conductive member 209 is disposed within the second conductive member 208 such that they are substantially coaxial (e.g. the major axis of the first conductive member and the major axis of the second conductive member are co-linear). In this 25 embodiment, the series inductance of the coaxial power connector assembly 203 is governed primarily by the basic equation:

$$L_{coax} = \frac{\mu_0 h}{2\pi} \ln(D_o/D_i)$$

where μ_0 is the permeability of space, h is the length of the power connector 203 body, D_O is the inner diameter of the outer conductor, and D_i is the diameter of the inner conductor. As the diameters get closer to each other the natural log function

5 approaches zero. This is the theoretical limit the inductance may achieve with such a construction. Practical issues limit achieving this limit however with such a construction the actual inductance achieved may be very low.

The reason for reducing the interconnection inductance is that the voltage drop across the interconnect is crucial for proper operation. As stated previously, high

10 current slew-rates can create large drops across an inductive interconnect. This may be seen by the simple equation for the dynamic voltage drop across an interconnect:

$$\Delta V \equiv I_{STEP} R_{AC} + L_{TOT} \frac{dI}{dt}$$

Where I_{STEP} is the step current the IC creates when switching transistors internally,

15 R_{AC} is the AC resistance of the interconnect, L_{TOT} is the total inductance of the interconnect, and dI/dt is the rate of change or AC current slew-rate which occurs due to the switching transistors. Often the inductance is the dominant element in the path and thus contributes to the largest portion of the drop across the interconnect.

20

Separable Coaxial Connector Embodiments

FIG. 3A is a diagram illustrating a preferred embodiment of a coaxial power connector assembly 300. The coaxial power connector assembly 300 is used to route power from a first circuit board to a second circuit board. In the illustrated embodiment the lower coaxial assembly 301 comprises a first conductive member such as an outer coaxial cylinder 303 and a second conductive member such as an inner coaxial cylinder 305. The outer coaxial cylinder 303 comprises first circuit board permanent attachment features such as lead extensions 304. In a preferred embodiment, the lead extensions 304 can be integrated with the outer coaxial cylinder

303, but this need not be the case. The lead extensions 304 electrically couple the outer cylinder to a first circuit board first power polarity, while the inner coaxial cylinder 305 with lead extensions 306 electrically couple the inner coaxial cylinder 305 to a first circuit board 315 second power polarity. Electrical coupling of the outer 5 coaxial cylinder 303 to a second circuit board first power polarity contact pad is accomplished by direct contact of the top end of the outer cylinder 303 to a first power polarity contact pad area on the second circuit board.

Disconnectable conduction features such as those on the Inner Diameter Contact Washer (IDCW) 302 are used to electrically connect the inner coaxial 10 cylinder 302 to a second circuit board second power polarity contact pad area utilizing spring contacts 307. The spring contacts 307 engage the inner diameter of the inner coaxial cylinder 305 and second surface 308 which engages a conductive surface (i.e. a second power polarity contact pad) on the second circuit board. In the illustrated embodiment, the IDCW is removably insertable into the inner diameter of the inner 15 coaxial cylinder 305 so that the contacts 307 press against the inner coaxial cylinder inner surface.

Side hole 309 in outer coaxial cylinder 303 is used to provide egress for dispensing insulating material between the outer coaxial cylinder 303 and the inner coaxial cylinder 305 and may be used for registering the inner and outer shells to each 20 other by placing holes in both the inner and outer shells and allowing material to flow into these holes thereby creating an alignment joint. This may also be accomplished by placing an insulating alignment pin into holes co-located with each other along the alignment pin axis.

FIG. 3B is a diagram revealing a more complete arrangement of the coaxial 25 power connector assembly 300 when used to route power between two circuit boards. In the illustrated embodiment lower coaxial assembly 301 is permanently attached to first circuit board 315 by solder methods utilizing plated thru holes (PTH) and circuit pads 316 and 317. Outer coaxial cylinder lead extensions 304 engage with PTHs 316

which are connected to the first power polarity circuit of first circuit board 315. Inner coaxial cylinder lead extensions 306 engage with PTHs 317 which are connected to the second power polarity circuit of first circuit board 315. Second circuit board 311 is shown as a flexible printed circuit board assembly consisting of at least two conductive planes 312 and 313. The lower plane 313 forms the first power polarity circuit in the second PCB 311 while the upper plane 312 forms the second power polarity circuit in the second PCB 311. The two planes are insulated from one another using a polyimide material 314B or other suitable electrical dielectric and their outer surfaces are protected from external damage by the use of an upper and lower cover layer 314A and 314C, respectively, also made of polyimide material or other suitable electrical dielectric. Note that power planes 312 and 313 are provided with a hole to allow the passage of IDCW 302 to pass through. Also note that cover layers 314A and 314C have been removed in the area proximate the coaxial cylinders so as to expose the power planes 312 and 313. Thus, as can be seen, upper portion of outer coaxial cylinder 303 is urged against second circuit board 311 first power polarity plane 313 creating a contact pad area to the plane at this junction. Next, lower surface 308 of IDCW 302 is urged against second power polarity plane 312 of second circuit board 311. A normal force applied to IDCW 302 causes the spring contacts 307 to be forced outward which, in turn, creates a contact to occur to the surface of the inner diameter of the inner coaxial cylinder 305. The required normal force which is applied substantially equally to both IDCW 302 in the area of lower surface 308 and the contact end of outer coaxial cylinder 303 is applied through screw fastener 319, washers 320 and 323, and captive nut 318 in PCB 315 which, collectively, provide the necessary normal force to urge IDCW 302 against second power polarity plane 312 and upper portion of outer coaxial cylinder 303 against first power polarity plane 313. Outer coaxial cylinder 303 is maintained separated from inner coaxial cylinder 305 by dielectric insulator 310. One method of fabricating such an insulator is to position the inner and outer cylinders 305 and 303 in a fixture and

inject a thermoplastic material through access hole 309. The thermoplastic material can be made to flow through to a second hole 321 in the inner coaxial cylinder 305 which can form a secondary feature 322 within the inner diameter of the inner coaxial cylinder 305. It should be noted that such secondary feature 322 is not necessary for 5 functionality of assembly 300 and may be useful only as a means of optimizing the manufacture of the dielectric feature 310. Furthermore, other methods of fabricating the coaxial structure 300 are possible.

FIG. 4A is a diagram of another embodiment of a coaxial power connector assembly 400. In this embodiment the outer coaxial cylinder 401 is similar to outer cylinder 303 with lead extensions 404 used to electrically couple the outer cylinder 401 to a first circuit board first power polarity (e.g. a circuit connector or trace in or on the first circuit board having a first power polarity or ground) and an inner coaxial cylinder 403 with lead extensions 405 used to electrically couple the inner cylinder 403 to a first circuit board second power polarity (e.g. a circuit connector or trace on 10 or in the second circuit board having a second polarity or ground). Electrical coupling of the outer coaxial cylinder 401 to a second circuit board first power polarity contact pad is accomplished by direct contact of the end 450 of the outer cylinder 401 to a first power polarity contact pad area on the second circuit board. Integral spring contact features 406 on inner coaxial cylinder 403 are used to electrically connect a 15 second circuit board second power polarity contact pad area. Dielectric insulating sleeve 402 provides separation of inner and outer coaxial cylinders 401 and 403. FIG. 20 4B illustrates assembly 400 in an assembled state.

FIG. 4C is a diagram revealing a more complete arrangement of the coaxial power connector assembly 400 when used to route power between two circuit boards. 25 In the illustrated embodiment coaxial assembly 400 is permanently attached to first circuit board 315 by soldering methods utilizing plated thru holes and circuit pads 316 and 317. Outer coaxial cylinder lead extensions 404 engage with PTHs 316 which are connected to the first power polarity circuit of first circuit board 315. Similarly, inner

coaxial cylinder lead extensions 405 engage with PTHs 317 which are connected to the second power polarity circuit of first circuit board 315. Upper portion of outer coaxial cylinder 401 is urged against pad 411 which is connected to first power polarity of second circuit board 407. Spring contacts 406 on inner coaxial cylinder 5 403 are urged against pad 410 which is connected to second power polarity of second circuit board 407, thus, completing the power circuit from first circuit board 315 to second circuit board 407. Screw fastener 408 and washer 409 are used to mechanically couple the second circuit board 407 to the first circuit board 315 through captive nut 318 in PCB 315. Note that spring contact 406 permits variations in height 10 differences between the inner coaxial cylinder 403 and outer coaxial cylinder 401 to be accommodated while maintaining controlled forces at both separable contact points on pads 410 and 411. If this were not the case and both cylinders were to simply be allowed to butt up against the contact pads small differences in cylinder heights could easily result in the shorter cylinder having an unreliable contact at its corresponding 15 pad on PCB 407.

FIG. 5A is an exploded view of a coaxial connector 500 where both the inner and outer conductive cylinders utilize spring contacts to engage a second circuit board with a separable connection. In this embodiment, the outer coaxial cylinder 503 has lead extensions 505 used to electrically couple the outer cylinder 503 to a first circuit 20 board first power polarity, and spring extensions 507 having contact areas 509 located at the opposite end of the spring extension 507 are used to establish a compliant and separable contact to second circuit board first power polarity via contact pads on the second circuit board. Similarly, inner coaxial cylinder 513 has lead extensions 515 used to couple electrically the inner cylinder to a first circuit board second power 25 polarity and spring extensions 516 with contact area 517 located at the end of the spring extension 516 used to establish a second compliant and separable contact to a second circuit board second power polarity again utilizing contact pads on second circuit board. Dielectric insulating sleeve 511 provides separation and electrical

isolation of inner 513 and outer 503 coaxial cylinders 503 and 513. Shroud 501 is used to provide support for spring extensions 507 and 516 when the assembly is compressed between the first and second circuit boards. Additionally, shroud 501 protects the contact ends 509 and 517 from damage prior to installation of the 5 assembly. Insulating standoff 519 is located within the inner coaxial cylinder 513 and is used to provide a limit stop on the 'z' axis separation between a first circuit board and second circuit board. Hole 521 in standoff 519 is used to accommodate a fastener which is used to join the two circuit boards and the coaxial connector 500. FIG. 5B illustrates assembly 500 when assembled.

- 10 FIG. 5C is a diagram revealing a more complete arrangement of the coaxial power connector assembly 500 when used to route power between two circuit boards. In the illustrated embodiment coaxial assembly 500 is permanently attached to first circuit board 315 by soldering methods utilizing plated thru holes and circuit pads 316 and 317. Outer coaxial cylinder lead extensions 505 engage with PTHs 316 which are 15 connected to the first power polarity circuit of first circuit board 315. Similarly, inner coaxial cylinder lead extensions 505 engage with PTHs 317 which are connected to the second power polarity circuit of first circuit board 315. Contacts 525 which are an extension of the body of outer cylinder 503 through spring 507 are urged against pads 525 which are connected to first power polarity of second circuit board 523.
- 20 Similarly, contacts 517 which are an extension of the body of inner cylinder 511 through springs 516 are urged against pads 527 which are connected to second power polarity of second circuit board 523. Note that termini of the spring contacts 509 and 517 share an approximate common diametrical circle and, thus, the contact pads 525 and 527 on the second circuit board 523 must alternate between the first power 25 polarity and the second power polarity. This arrangement referred to as an interdigitated connection is very beneficial in reducing the interconnection inductance of the power circuit. Screw fastener 408 and washer 409 are used to mechanically couple the second circuit board 523 to the first circuit board 315 through captive nut

318 in PCB 315. Spacer 519 establishes a precise separation 'z' axis between PCBs 523 and 315 which results in controlled contact forces at pads 525 and 527. As previously noted, shroud 501 helps support spring extensions 507 and 516 when PCBs 523 and 315 are urged together.

5

Conclusion

This concludes the description of the preferred embodiments of the present invention. In summary, the present invention describes a method, apparatus, and article of manufacture for providing power from a first circuit board to a second circuit board. The apparatus comprises a first conductive member, including a first conductive member first end and a first conductive member second end distal from the first end; a second conductive member disposed within the first conductive member, the second conductive member including a second conductor member first end and a second conductor member second end distal from the second conductor member first end; and one or more first circuit board permanent attachment features for electrical coupling with the first circuit board and second circuit board, and one or more disconnectable conduction features for electrically coupling the connector with the second circuit board. One of the advantages of the present invention is the integration of function in which the apparatus operates both as a rigid standoff to separate the first circuit board from the second circuit board, and a conduit for delivering power and a ground return between the circuit boards as well. While the apparatus will be discussed in terms of providing a power signal from a first circuit board to a second circuit board, it can also be used to provide power to a plurality of circuit boards in a stacked configuration, all with minimal interconnect impedance.

The foregoing description of the preferred embodiment of the invention has been presented for the purposes of illustration and description. It is not intended to be

exhaustive or to limit the invention to the precise form disclosed. Many modifications and variations are possible in light of the above teaching. It is intended that the scope of the invention be limited not by this detailed description, but rather by the claims appended hereto. The above specification, examples and data provide a complete 5 description of the manufacture and use of the composition of the invention. Since many embodiments of the invention can be made without departing from the spirit and scope of the invention, the invention resides in the claims hereinafter appended.

CLAIMS

What is Claimed is:

1. A connector, for providing power from a first circuit board to a second circuit board, comprising:
 - 5 a first conductive member, including a first conductive member first end and a first conductive member second end distal from the first end;
 - a second conductive member disposed within the first conductive member, the second conductive member including a second conductor member first end and a second conductor member second end distal from the second conductor member first end; and
 - 10 one or more first circuit board permanent attachment features for electrical coupling with the first circuit board and second circuit board, and one or more disconnectable conduction features for electrically coupling the connector with the second circuit board.
- 15 2. The connector of claim 1, wherein:
 - the one or more first circuit board permanent attachment features for electrical coupling with the first circuit board is disposed at one or both of the first conductive member first end and the second conductive member first end; and
 - 20 the second circuit board disconnectable conduction features for electrically coupling the connector with the second circuit board are disposed at one or both of the first conductive member second end and the second conductive member second end.
- 25 3. The connector of claim 2, wherein:
 - the first circuit board permanent attachment features comprises lead extensions from the one or both of the first conductive member first end and the second conductive member first end.

4. The connector of claim 3, wherein the lead extensions are integrated with the one or both of the first conductive member first end and the second conductive member first end.

5 5. The connector of claim 3, wherein the lead extensions are disposed in holes in the first circuit board.

6. The connector of claim 3, wherein the lead extensions are disposed substantially in a z axis normal to the first circuit board

10

7. The connector of claim 2, wherein the second circuit board disconnectable conduction features comprises spring contacts.

15

8. The connector of claim 7, wherein the spring contacts are integrated with the one or both of the first conductive member second end and the second conductive member second end.

20

9. The connector of claim 2, wherein the second circuit board disconnectable conduction features comprise spring contacts removably insertable into an inner diameter of the second conductive member and pressing against the inner diameter of the second conductive member.

25

10. The connector of claim 9, wherein at least one of the spring contacts comprise a surface parallel to and electrically coupling with a conductive surface of the second circuit board.

11. The connector of claim 10, wherein the conductive surface of the second circuit board is disposed on a top side of the second circuit board opposite the first conductive member.

5 12. The connector of claim 10, wherein the conductive surface of the second circuit board is disposed on a bottom side of the second circuit board.

13. The connector of claim 2, wherein the second circuit board disconnectable conduction features comprises:

10 first conductive member disconnectable conduction features disposed at the second end of the first conductive member;
second conductive member disconnectable conduction features disposed at the second end of the second conductive member; and
the first conductive member disconnectable conduction features are
15 interdigitated with the second conductive member disconnectable conduction features.

14. The connector of claim 13, wherein the first conductor disconnectable conduction features are alternatively interdigitated with the second conductive member disconnectable conduction features.

20 15. The connector of claim 13, further comprising a shroud, substantially surrounding the first conductive member.

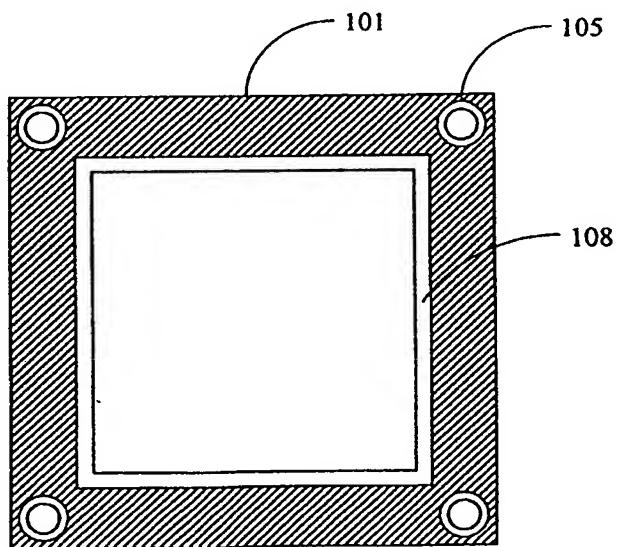
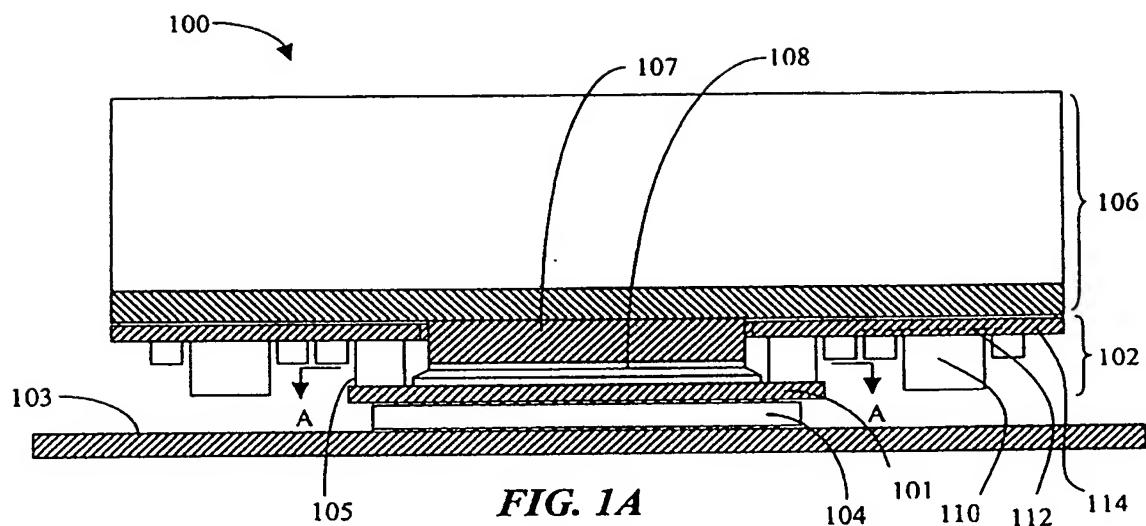
16. The connector of claim 2, wherein the second circuit board
25 disconnectable features are compressible in a z-axis normal to the first circuit board and the second circuit board and accommodate differences between a length of the first conductive member and the second conductive member.

17. The connector of claim 16, wherein the first conductive member is shorter than the second conductive member.

18. The connector of claims 16, further comprising a standoff disposed
5 within the second conductive member.

19. The apparatus of claim 2, further comprising a fastener disposed through the second conductive member, the fastener urging the first and the second circuit boards together.

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**FIG. 1B**

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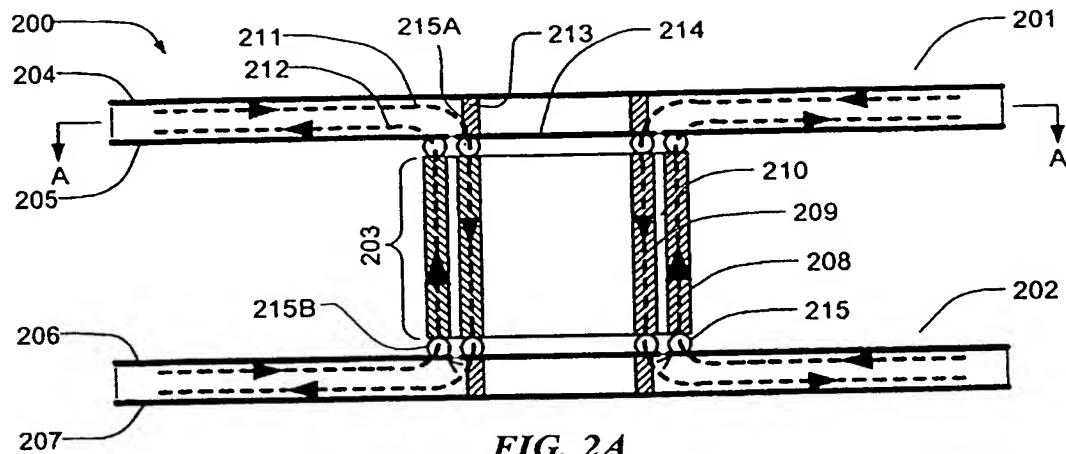
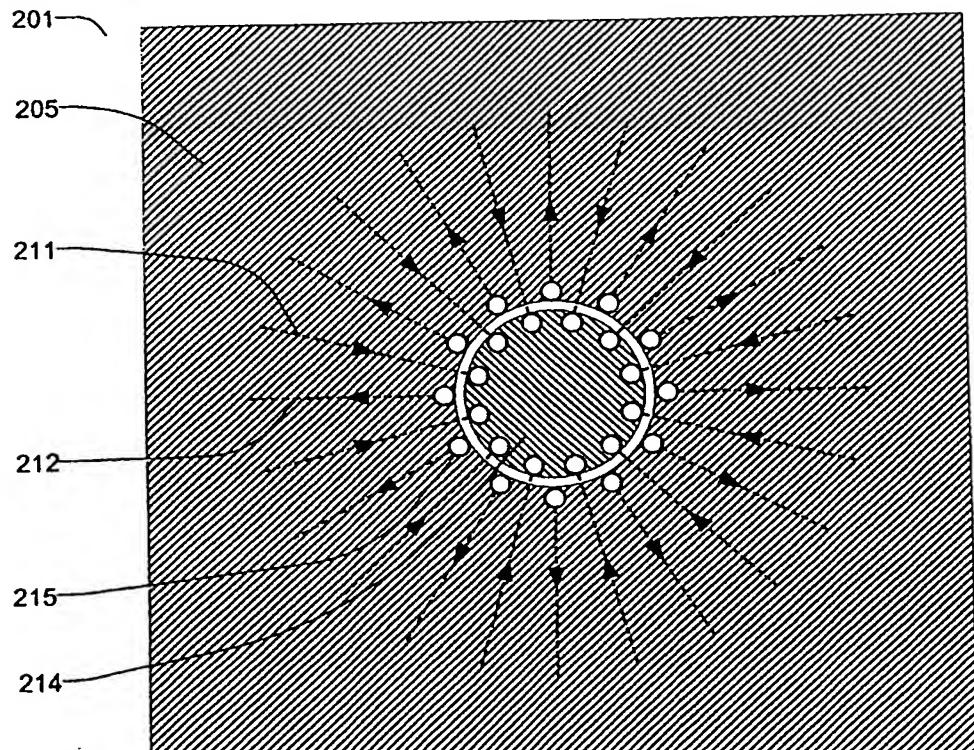


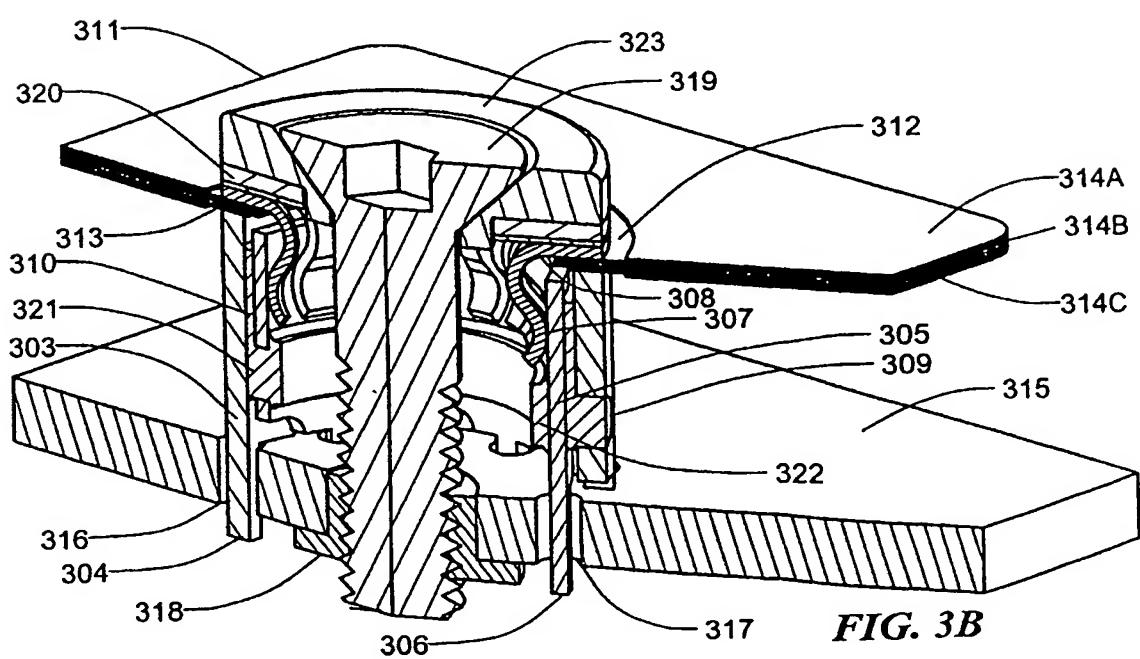
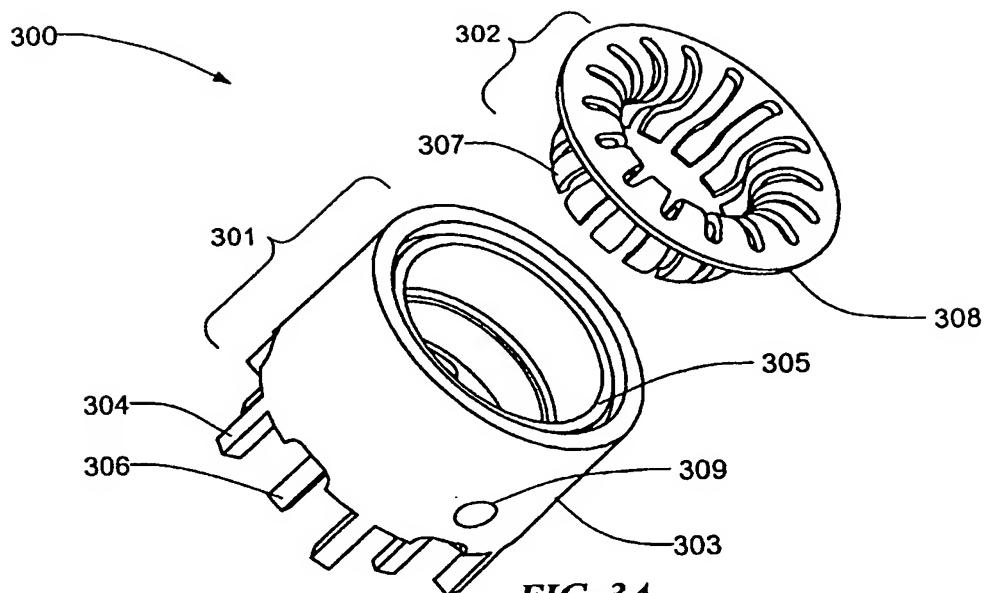
FIG. 2A



Section A-A

FIG. 2B

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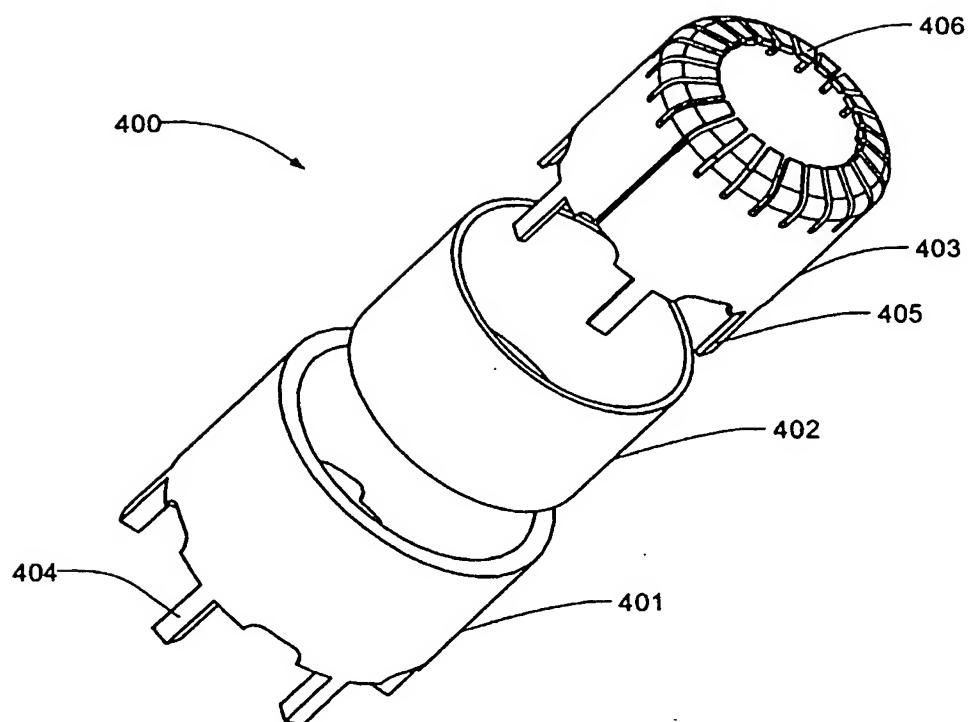


FIG. 4A

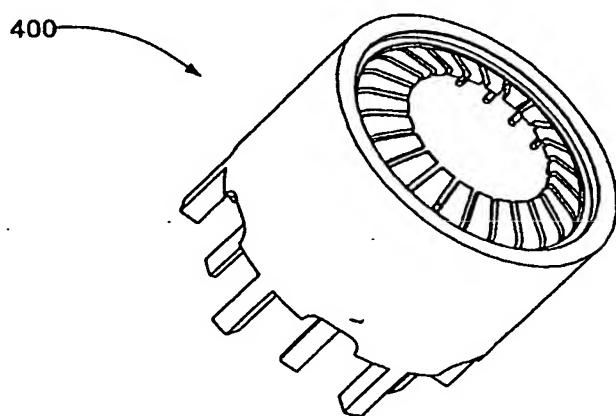


FIG. 4B

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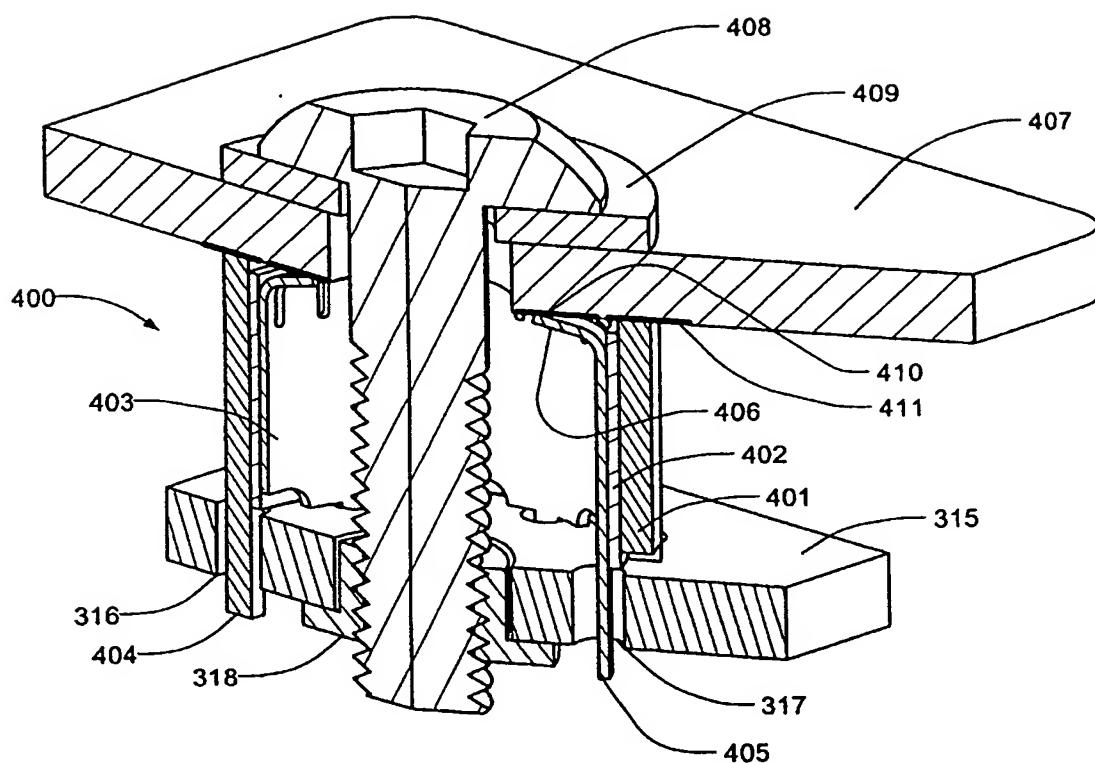
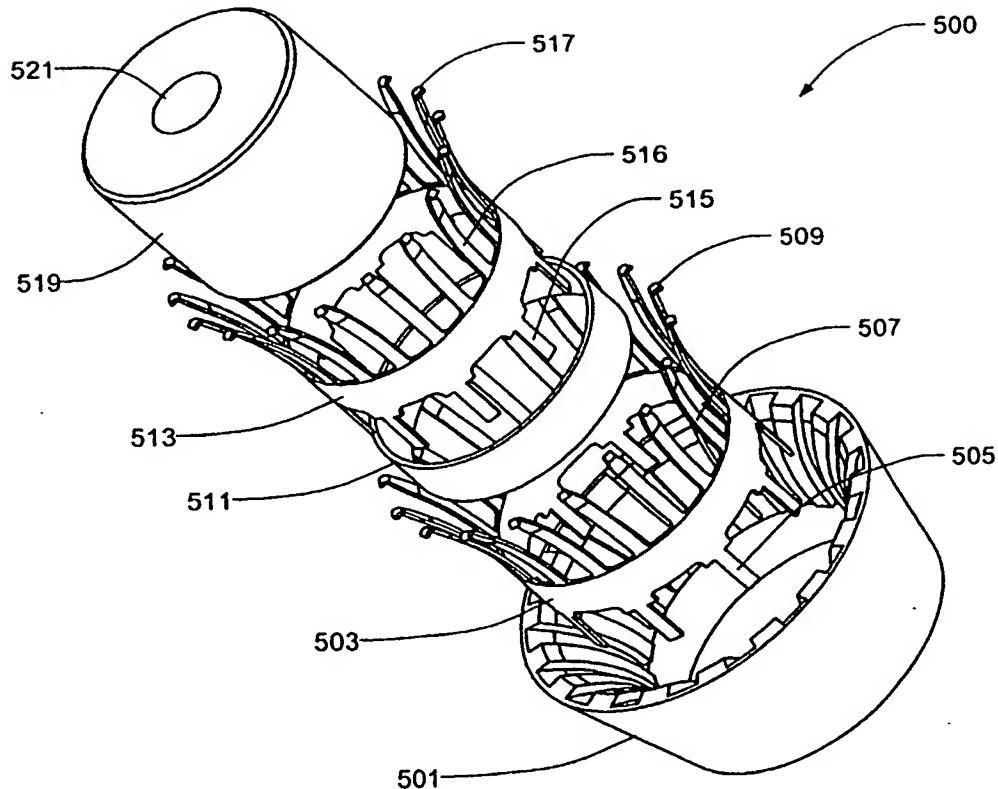
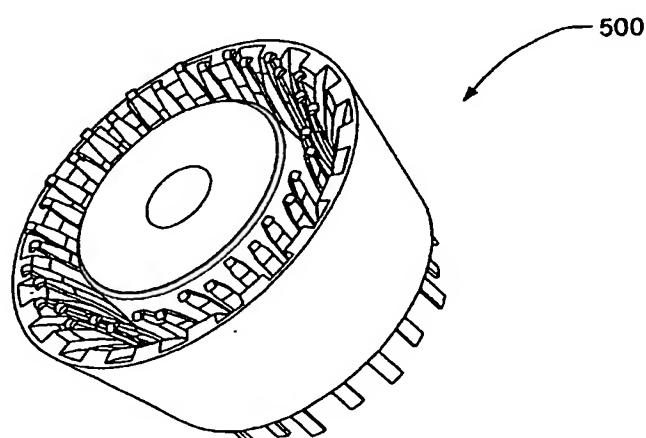
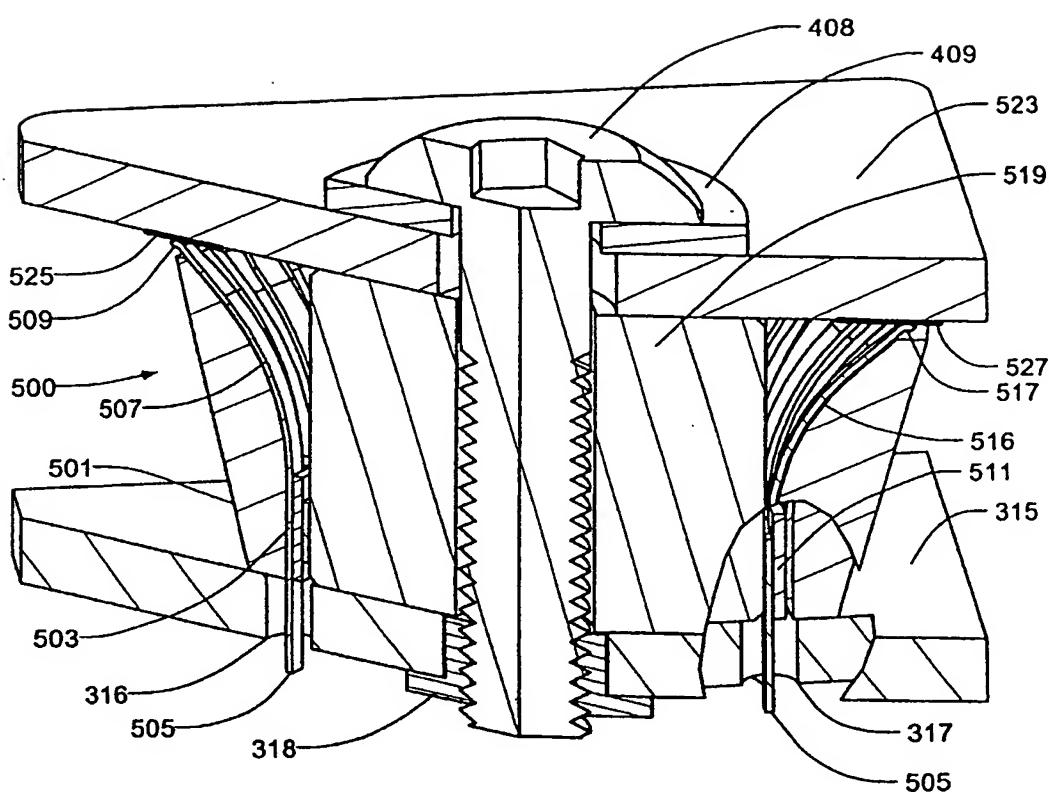


FIG. 4C

6/7**FIG. 5A****FIG. 5B**

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**FIG. 5C**